

# An Improved Metric for the Sooting Propensity of Fuels

Roger Watson

Chris Ness

Rui Hu

Andrew Smallbone

Neal Morgan

Markus Kraft

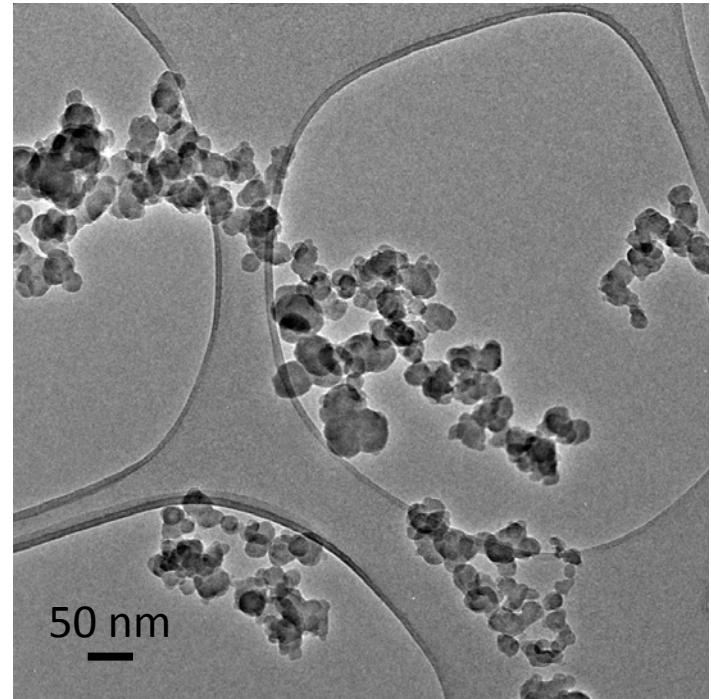


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# Background

- We all know soot is bad for health and the environment
- Two key questions:
  - What kind of soot do different fuels produce under different circumstances?
  - **How much soot do they produce?**

Soot agglomerate from the soot trail of a toluene laminar diffusion flame above its smoke point. Sample taken by R Watson; image by C Ducati.



**CoMo  
GROUP**

Dr Roger Watson  
[rw406@cam.ac.uk](mailto:rw406@cam.ac.uk)



# The Threshold Sooting Index (TSI)

- Standard metric for the sooting propensity of a fuel
- Can be obtained from laminar diffusion or premixed flames
- Usually obtained from the ‘smoke point’ or the ‘critical equivalence ratio’ [Calcote & Manos]
- Typically given by correlations of the form:

$$TSI = b \pm ax$$

(where a and b are empirical coefficients and x is a simple function of the measured parameter).

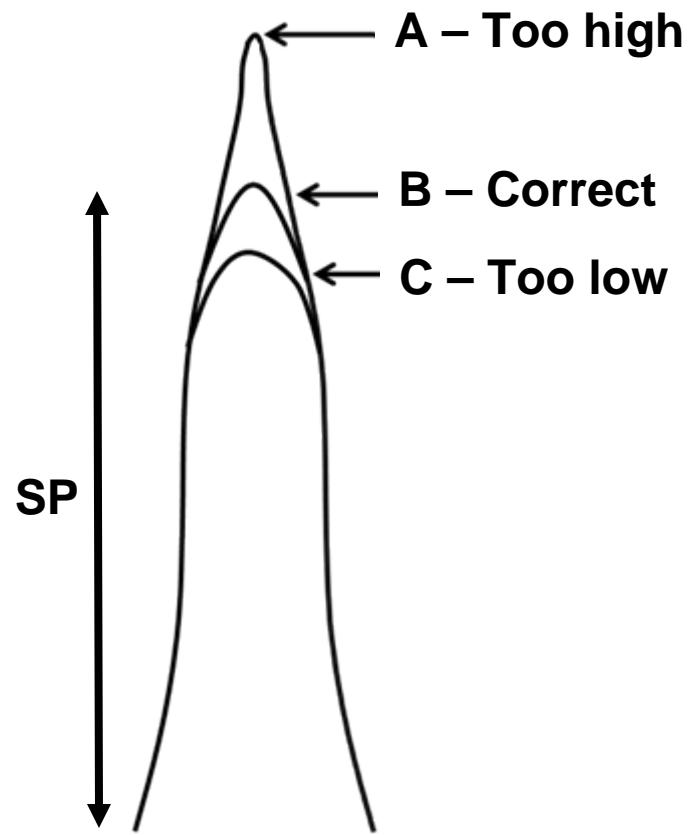
- Shown to correlate well with soot emissions from real combustors [Yang, Boehman & Santoro]



# The Smoke Point test

- ASTM D1322 criterion is the most commonly used
- Identifies smoke point with a specific flame morphology
- Highly subjective
- Smoke point converts to TSI using:

$$TSI = a \left( \frac{MW}{SP} \right) + b$$



# Converting to TSI

- Choose two reference fuels based on literature data.  
For example:
  - TSI (methylnaphthalene) = 100
  - TSI (methylcyclohexane) = 5
- Use your apparatus to determine the smoke point of these reference fuels experimentally.
- Determine the apparatus-dependent coefficients  $a$  and  $b$  by simultaneous solution:

$$a = \frac{TSI_1 - TSI_2}{\left( \frac{MW_1}{SP_1} \right) - \left( \frac{MW_2}{SP_2} \right)}$$

$$b = \frac{TSI_1 \left( \frac{MW_2}{SP_2} \right) - TSI_2 \left( \frac{MW_1}{SP_1} \right)}{\frac{MW_2}{SP_2} - \frac{MW_1}{SP_1}}$$

- In practice, the error margin in the TSI is typically at least 15% and can be much higher – not good!



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[rw406@cam.ac.uk](mailto:rw406@cam.ac.uk)



# Alternative method

- Use the fuel uptake rate at the smoke point to characterise sooting propensity instead [Olson & Pickens]
- Uptake rate was thought to be less sensitive to flame height around the smoke point, meaning that readings might be more reproducible
- The following equation was suggested:

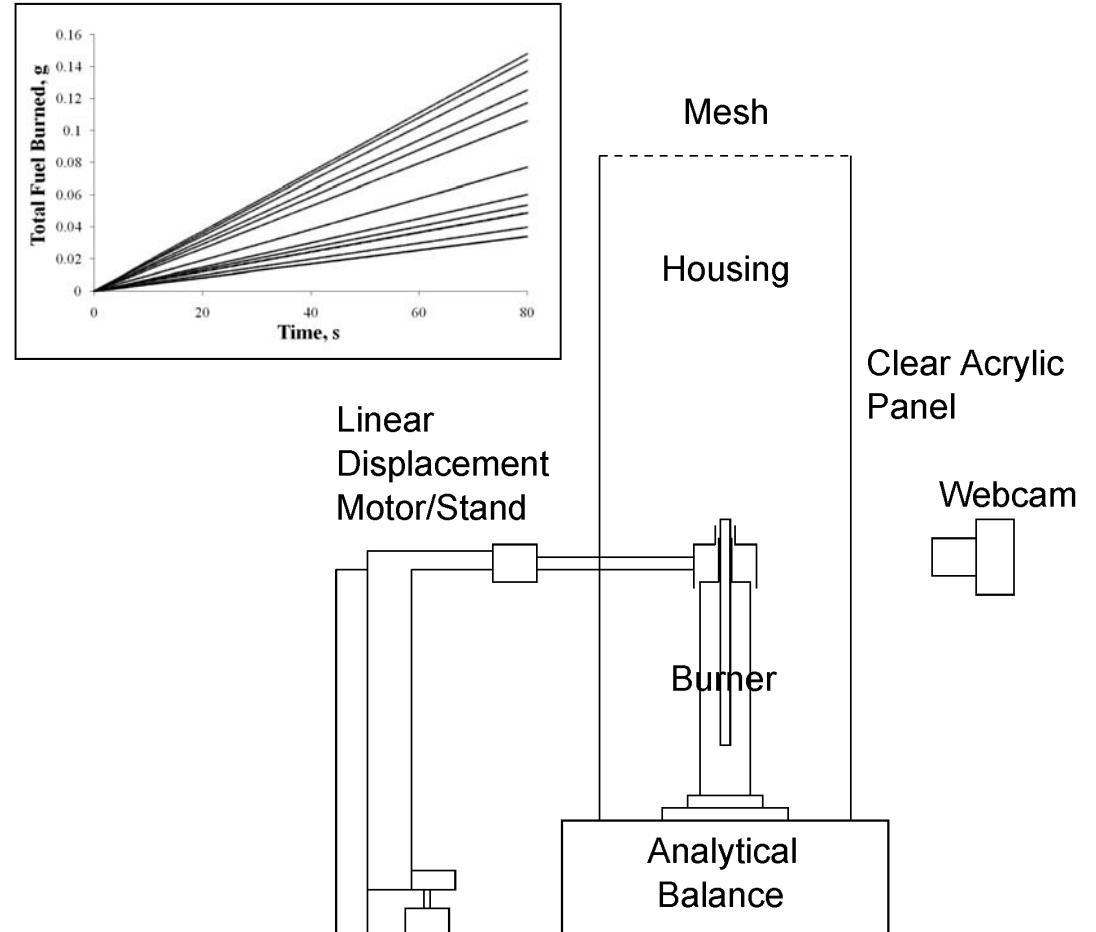
$$TSI = a \left( \frac{MW}{\dot{m}} \right) + b$$

- Is this really an improvement?

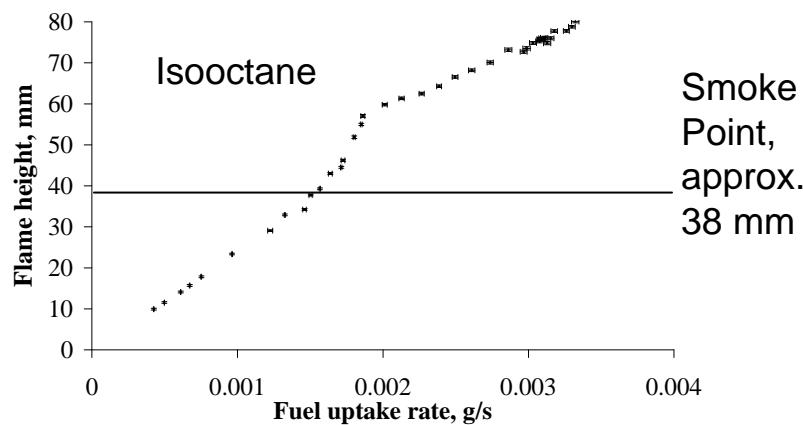
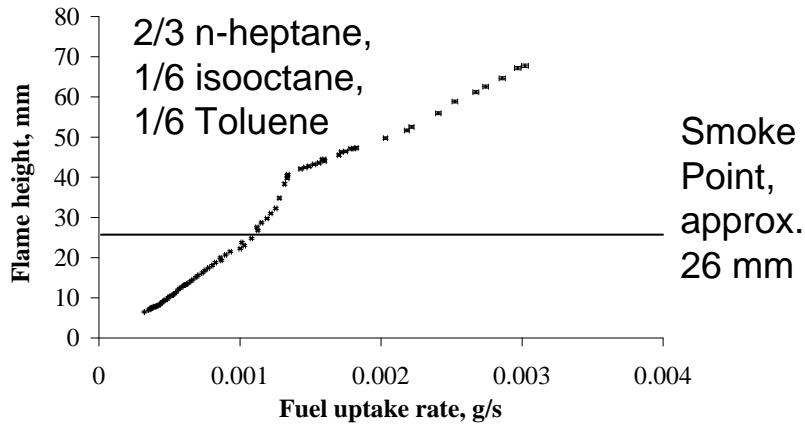
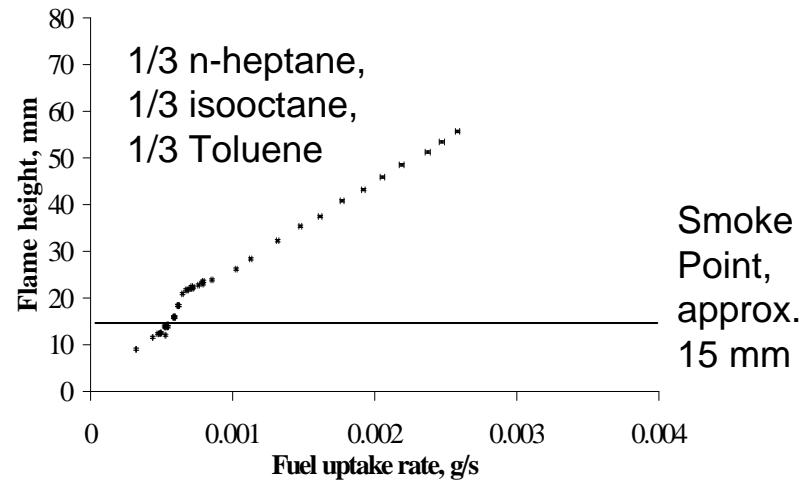
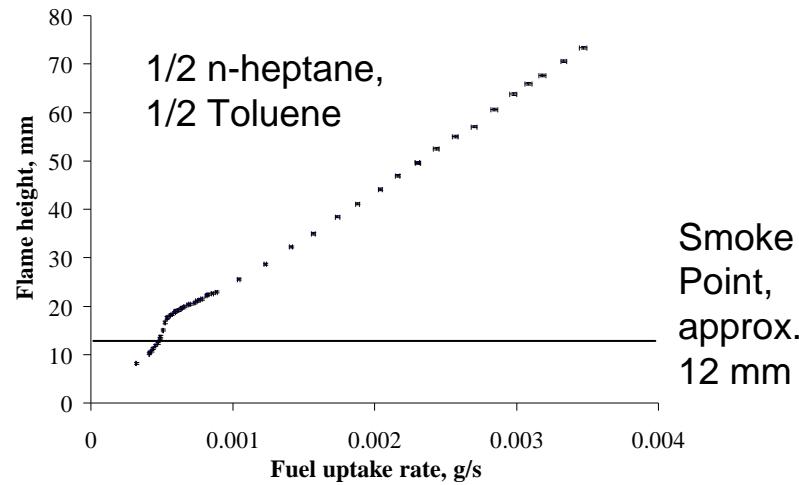


# Understanding the Smoke Point

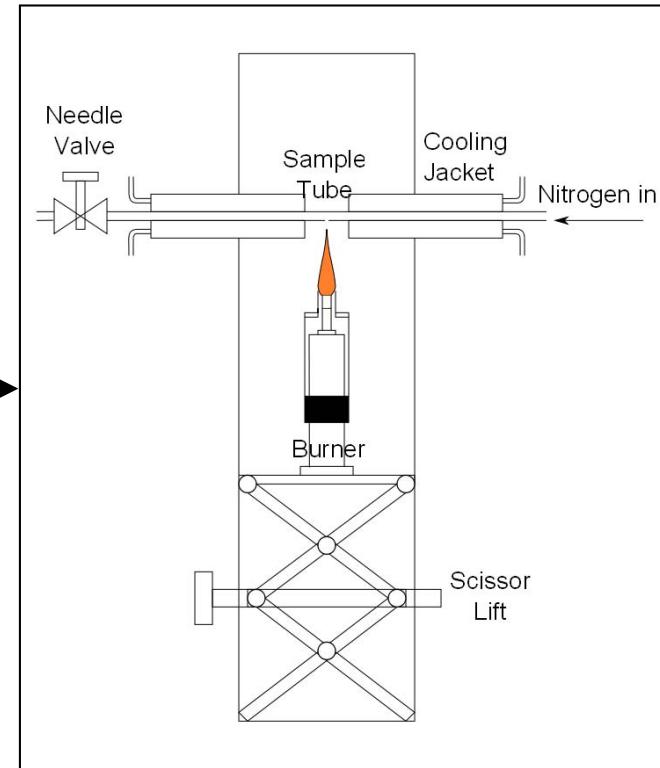
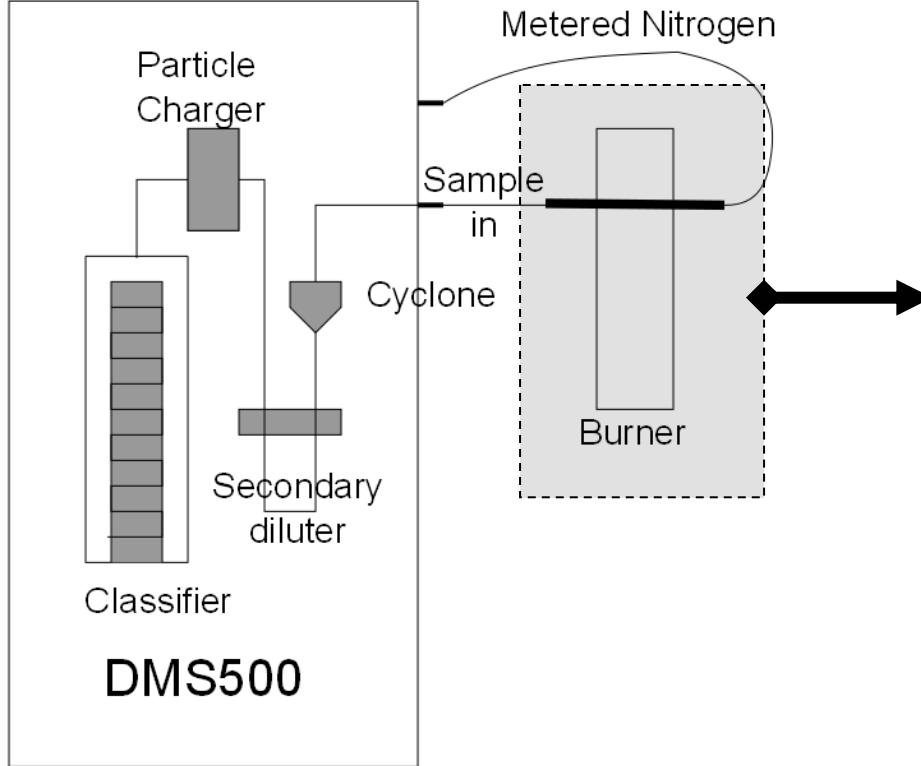
- Used ASTM burner with modified housing to measure fuel uptake rate vs flame height
- Flame height from video camera & MATLAB image analysis
- Uptake rate from analytical balance readings



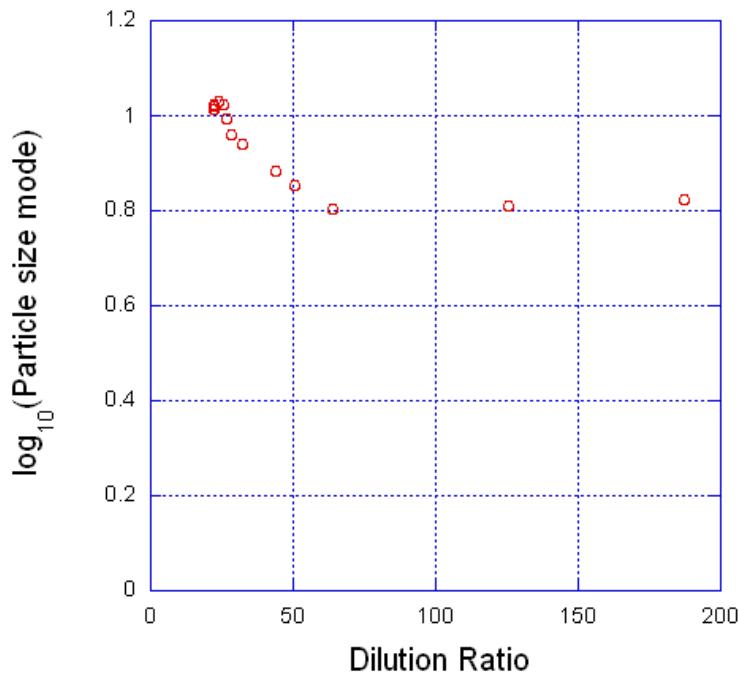
# Flame height vs Fuel Uptake Rate



# PSD measurement Apparatus



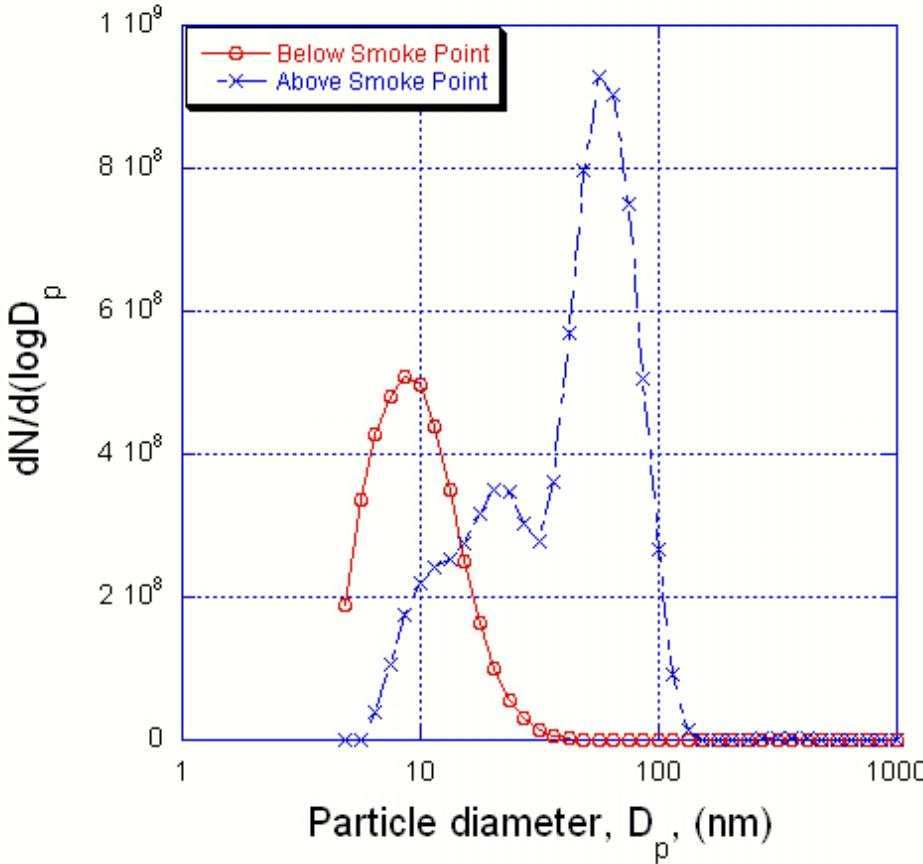
# Sample Dilution



- Effects of oxidation, surface reaction and coagulation mitigated by diluting the sample with nitrogen
- Dilution ratio was adjusted using a needle valve, which decreased the sample line vacuum
- PSD was found to be independent of dilution when the dilution ratio was higher than about 50-100



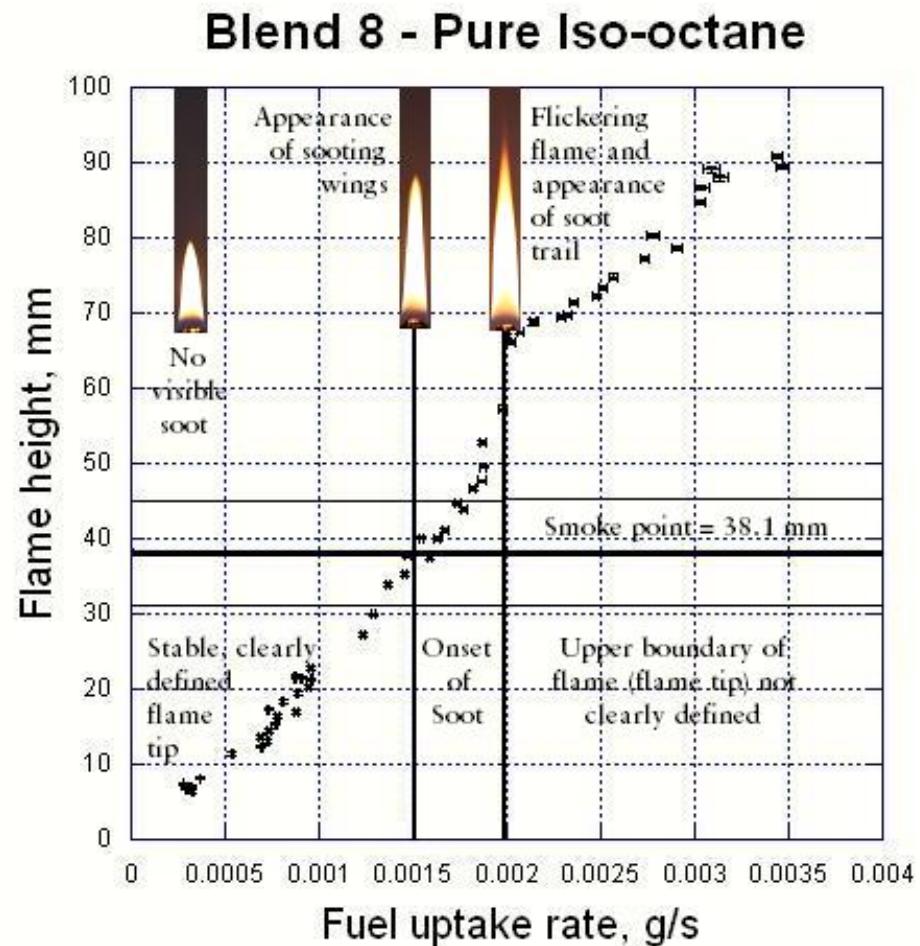
# PSD above smoking & non-smoking flames



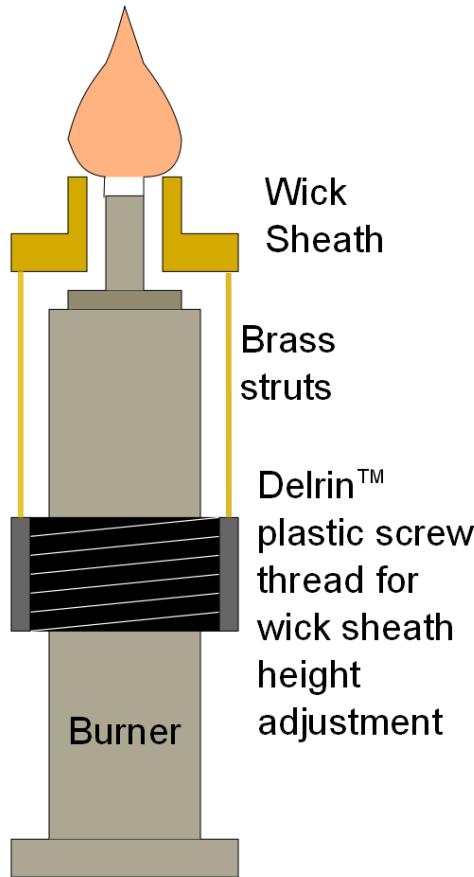
- Very difficult to get repeatable results because of high particle number concentration gradients; needs precise positioning and a very stable flame
- Clear shift from single mode (volatiles?) to multi-mode PSD when a soot trail is visible

# Findings

- Fuel uptake rate vs flame height curve always showed a distortion just above the smoke point
- Relationship is still almost linear at the smoke point itself
- Lowest sensitivity to flame height occurs just prior to the appearance of a soot trail - Measure uptake rate here instead!



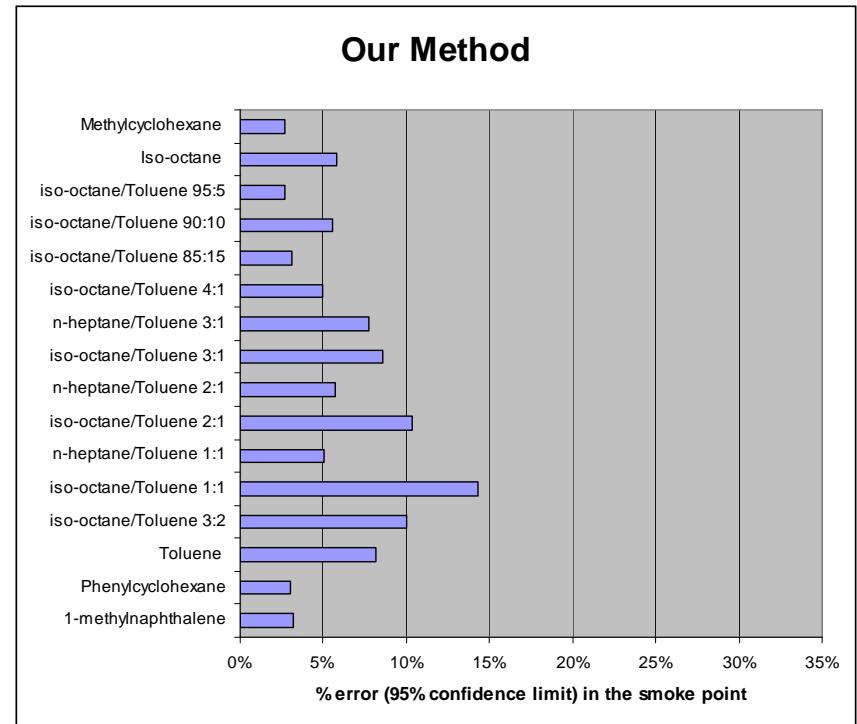
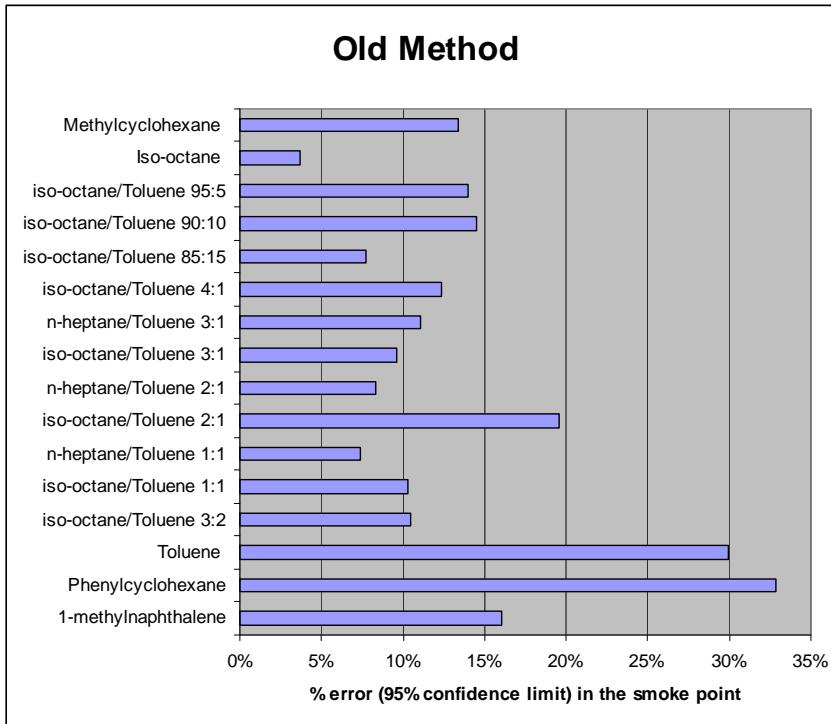
# Lightweight Burner Design



- **Our Method:** Need to measure fuel uptake rate at incipient formation of soot trail by weighing burner
- Burner mass must not exceed the balance rating
- Lightweight burner was designed for quick and easy measurements, with rapid changeover of fuels

# Testing a New Method

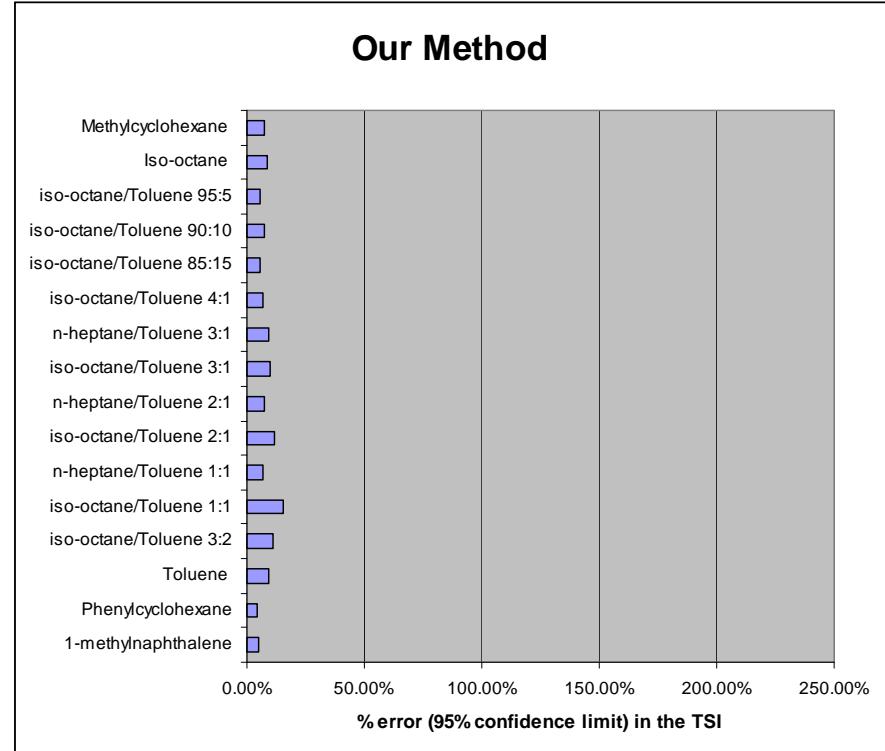
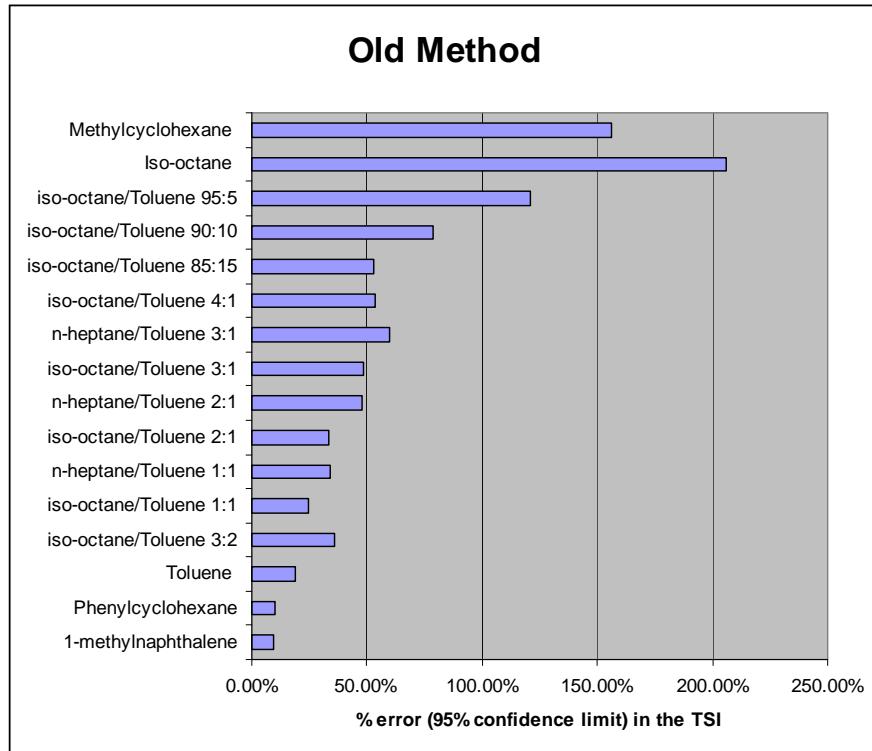
Smoke point errors estimates based on 9 measurements between at least two different experimentalists



**Experimental uncertainty in raw data has been halved!**



# Error in the TSI



$$TSI = a\left(\frac{MW}{SP}\right) + b$$

$$TSI = a\left(\frac{MW}{m}\right) + b$$

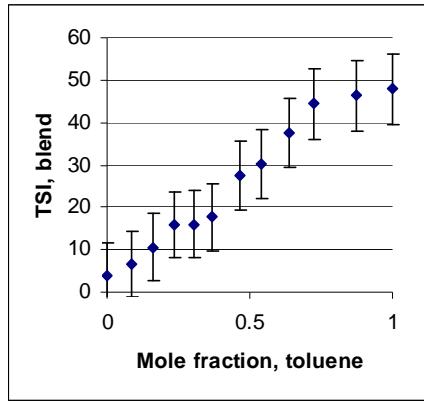
Includes error in determining coefficients  $a$  and  $b$



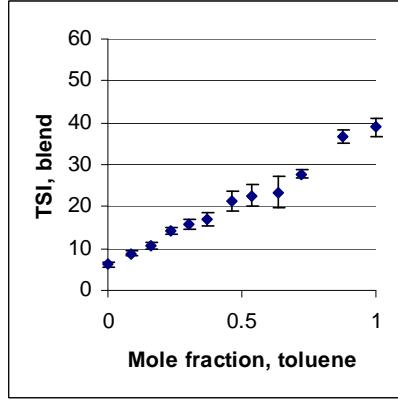
# Conversion to TSI – Linear Blending?

Isooctane  
+ toluene

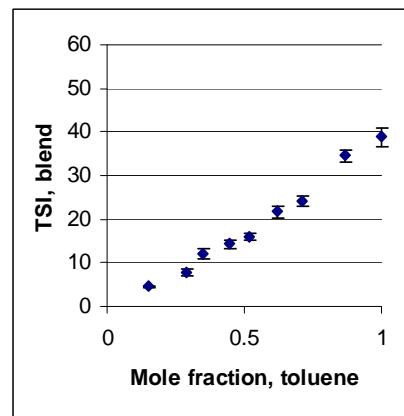
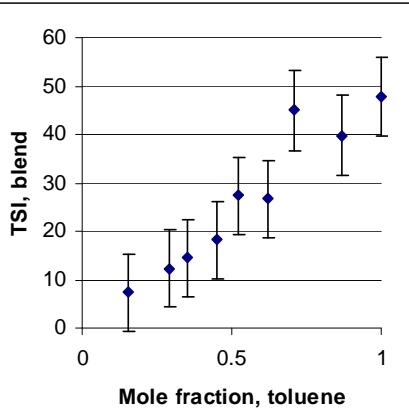
ASTM Method



Our Method



n-heptane  
+ toluene



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Dr Roger Watson  
rw406@cam.ac.uk



# Conclusions

- Much better TSI reproducibility is achieved by basing it on fuel uptake rate at the point of incipient soot trail formation instead of the smoke point
- The best correlation for TSI seems to be:

$$TSI = a\left(\frac{MW}{\dot{m}}\right) + b$$

- Confirmed that TSIs blend almost linearly with mole fraction, although there might be slight curvature



# References

- H. F. Calcote and D. M. Manos. Effect of molecular structure on incipient soot formation. *Combustion and Flame*, 49(1-3):289–304, 1983. doi:10.1016/0010-2180(83)90172-4
- Y. Yang A. L. Boehman and R. J. Santoro. A study of jet fuel sooting tendency using the threshold sooting index (tsi) model. *Combustion and Flame*, 149(1-2):191–205, 1985.
- D. Olson, J. Pickens, and R. Gill. The effects of molecular structure on soot formation II. diffusion flames. *Combustion and Flame*, 62(1):43–60, 1985.



# Acknowledgements



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Dr Roger Watson  
[rw406@cam.ac.uk](mailto:rw406@cam.ac.uk)

