Cold Start DI Gasoline Particulate Emissions



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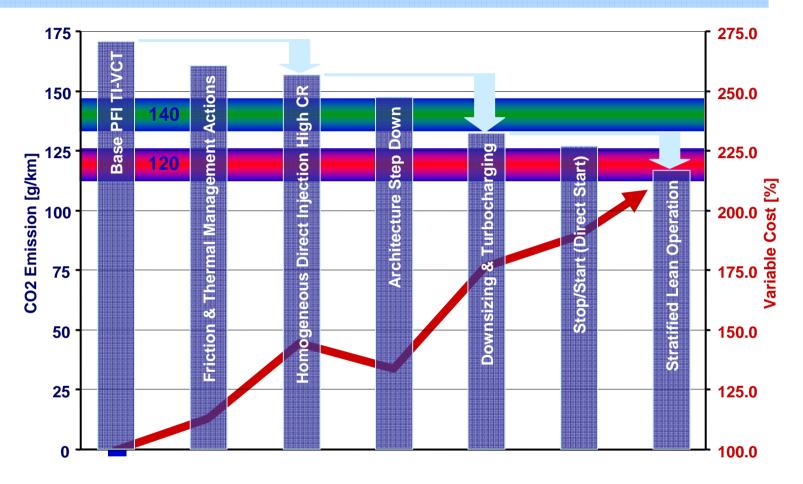


Summary

- 1. Background: DI Gasoline Engines, their PM Emissions and Cold Start Effects
- 2. Experimental Details: Hardware, Sampling system and Measurement of PM Emissions
- 2. HC Emissions and their Temperature Dependence
- 3. PM Size Distributions and Composition (Thermo-gravimetric Analysis)
- 4. Volatile PM Analysis (Thermo-gravimetry)
- 5. PM Geometrical Size and Morphology (HR TEM & DMS500)



CO₂-Reduction Strategy Example



- ACEA commitment requires CO₂ reduction
- c40% CO₂ reduction possible through combination of above technologies

Figure from Martin Wirth: 27. International Vienna Engine Symposium 2006 Cambridge Particles Meeting. 18 May 2007



Background – Comparison of DI to Port Fuel Injection

- Lower throttling loss: Stratified charge mode, higher EGR tolerance, (downsizing)
- Higher specific power output: enables downsizing
- Faster catalyst light-off: split injection \rightarrow large exhaust heat fluxes
- Improved fuel metering control, better droplet atomization, improved transient response
- Synergies with downsizing and forced induction:
 - Higher specific power output due to charge cooling effect on volumetric efficiency
 - higher CR improves low end torque in forced induction applications



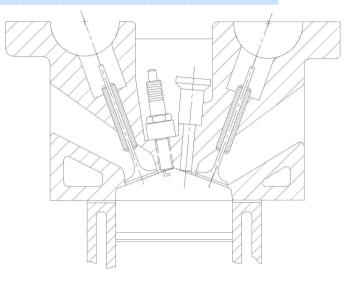
Background – DI Gasoline PM Emissions

Second Generation DI Combustion System

Closely spaced centrally mounted injector and spark plug. Flat top piston.

Factors that influence PM Emissions:

- Reduced time available for mixture preparation
- Piston and liner wetting



→ Local oxygen privation either close to surfaces or around incompletely vaporised fuel droplets → formation of elemental carbon particles

- Since the above are local effects only, soot emission rates are normally lower than from compression ignition engines

- At low loads: High saturation ratios for condensable species and comparatively low total soot surface means that the condensed organic <u>fraction</u> can be a significant contribution to the emitted PM

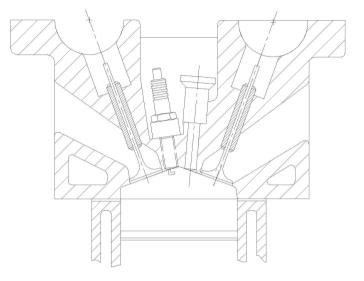


Background – Mixture Preparation and Cold Starts

In SI engines, PM emissions have a strong dependence on mixture preparation:

- incomplete evaporation
- presence of fuel droplets
- fuel films on surfaces
- AFR Stratification
- Worsened by:
- Downsizing (higher internal loads)
- Forced induction (more fuel to evaporate)
- Biofuel blends (higher Δh_{fg} and lower calorific values)
- **Cold starts** (Habchi et. al: up to 25% of the injected fuel mass on surfaces)

Habchi *et. al.* Influence of the Wall Temperature on the Mixture Preparation in DI Gasoline Engines. Oil and Gas Science and Technology – Rev. IFP, Vol 54 (1999), No.2 pp211 – 222.





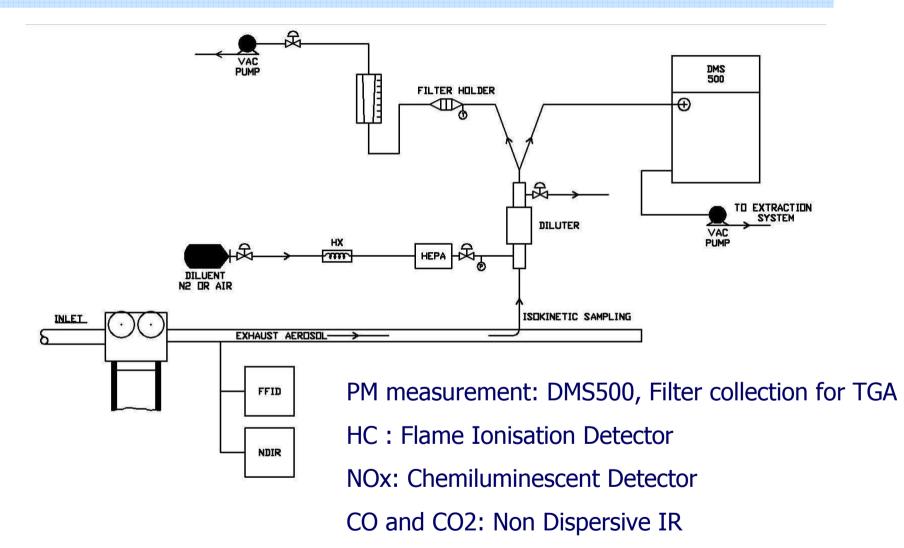


Test Matrix and Engine Specification

Engine type	4 Stroke	Test	AFR	Fuel Pressure (bar)	Start of Injection (CAD bTDC)
Combustion system	Spray Guided Direct Injection				
Bore x stroke	89 x 90 mm				
Swept volume	562 cm ³	А	12	50	300
Compression ratio	9.5:1	В	12	50	240
Injector type	Solenoid Multi-hole Nozzle (150 bar)	С	12	150	300
Engine speed	1750 rpm	D	12	150	240
Inlet manifold pressure	1.0 bar	E*	14	100	270
		F	16	50	300
Nominal indicated mean effective pressure	9.0 bar	G	16	50	240
		Н	16	150	300
Fuel	Unleaded Gasoline	I	16	150	240

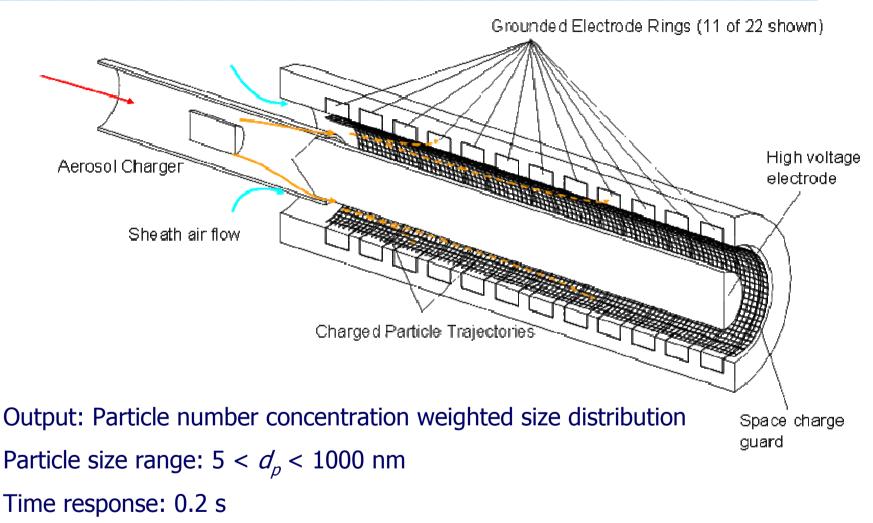


Experiment





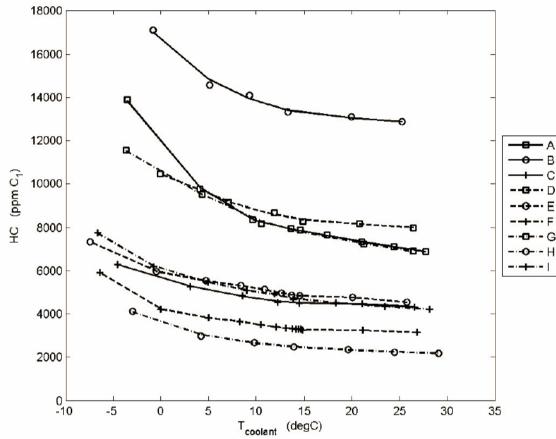
Electrical Mobility Classification



Reavell et. al. SAE 2002-01-2714,

Symonds et. al. Aerosol Science 38 (2007) pp 52-68.

Results: Feed-gas HC Emissions vs Temp



[HC] higher at cold temperatures because:

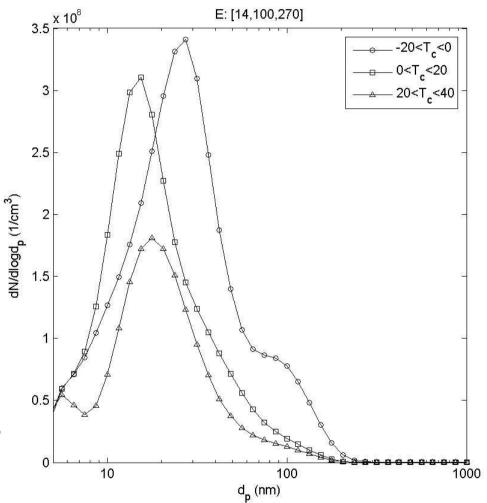
- increased flame quenching at low T because the thermal boundary layer is thicker.
- Increased absorption of fuel to the lube oil layer on liner surface.
- Larger crevice volumes





PM Dependence on Coolant Temperature

Thermo-gravimetric Analysis		
	PM Mass Fraction (%)	
Light Organic	44.3	
Heavy Organic	42.9	
EC	12.8	

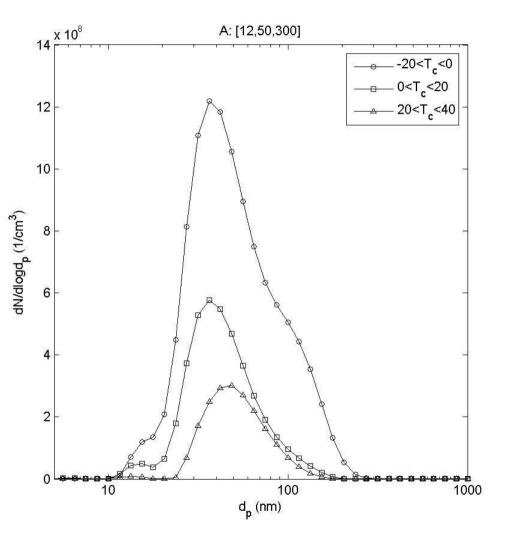


 $N_{[5-1000nm]} = 1.6E8 \text{ particles/cm3}$



PM Dependence on Coolant Temperature

Thermo-gravimetric Analysis		
	PM Mass Fraction (%)	
Light Organic	66.0	
Heavy Organic	8.5	
EC	25.5	

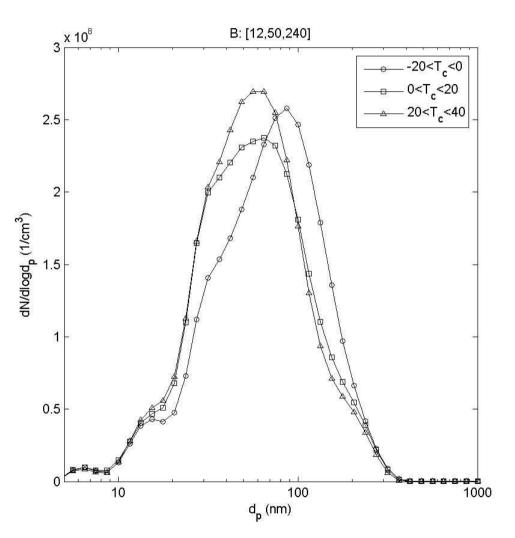


 $N_{[5-1000nm}] = 1.8E8 \text{ particles/cm3}$



PM Dependence on Coolant Temperature

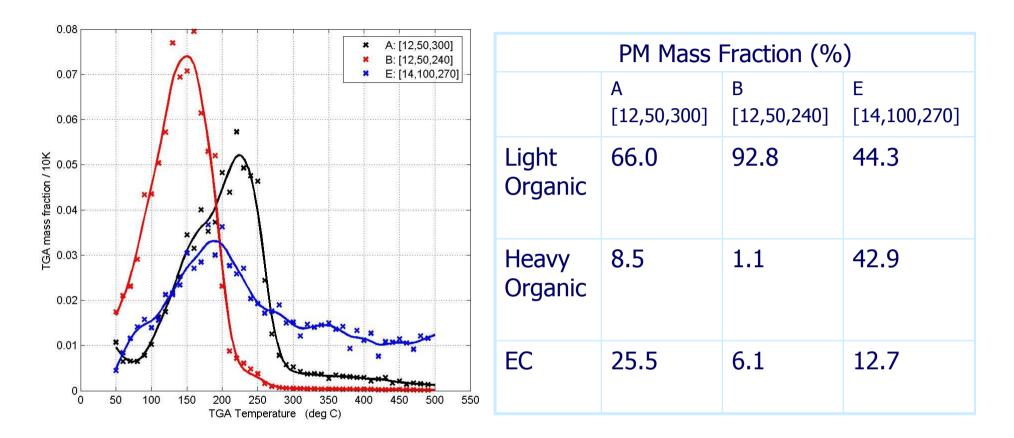
Thermo-gravimetric Analysis		
	PM Mass Fraction (%)	
Light Organic	92.8	
Heavy Organic	1.1	
EC	6.1	



N_[5-1000nm] = 1.9E8 particles/cm3



Thermo-gravimetric Analysis of Volatile PM

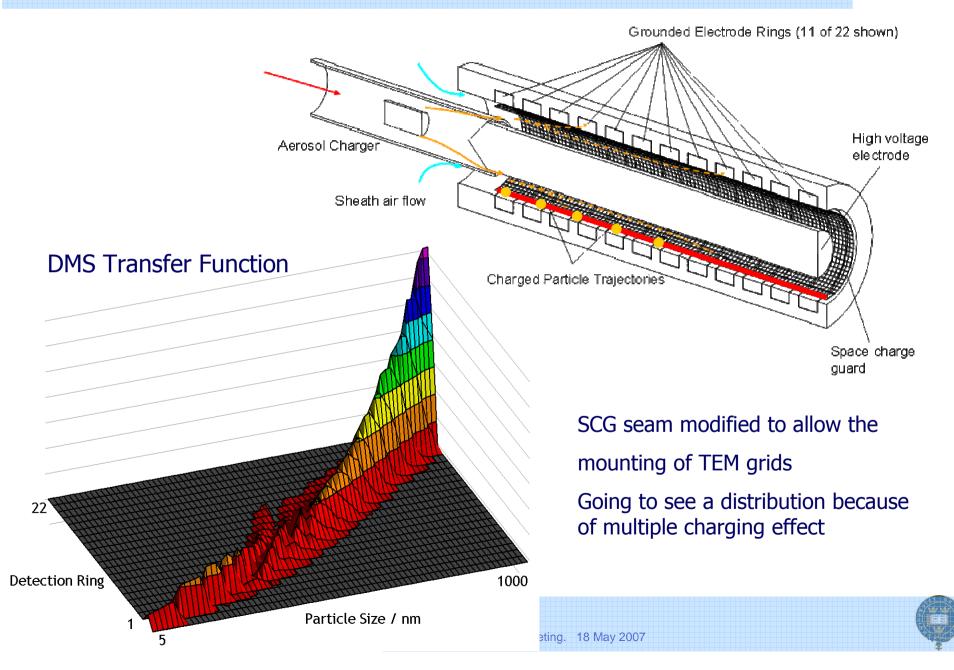


-Normalised with total volatile mass

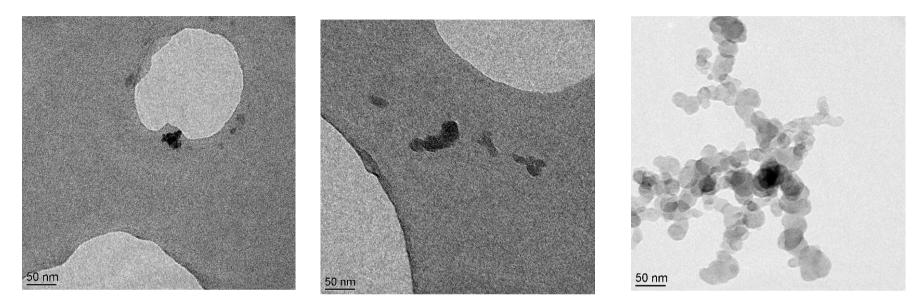
- Dominated by light material (leaves TGA ~< 300 degC)



Space Charge Guard Modifications



High Res Transmission Electron Microscopy



Transmission Electron Micrographs of Sub-micron particles from gasoline combustion.

Shown: Elemental Carbon Particles.

Not Shown: Volatile Organics

Inorganics: Sulphate and Nitrate anions, ash residues (metals)





Conclusions

DI Gasoline Engine, Cold Start, Full Load PM Measurements made with DMS500, TGA and TEM

- M Thermo-gravimetric analysis showed that the composition of the emitted PM was dominated by volatile material. The elemental carbon fraction did not exceed c30 percent of the total PM by mass.
- ▲ Transmission electron microscopy confirmed the presence of a variety of solid particles, ranging from a c20 nm in diameter for single particles to a few hundred nm for aggregates. Elemental carbon particles of both amorphous and partly graphitised microstructures were detected.
- ➢ Following a cold start from -10 °C, PM number concentration generally decreased with increasing coolant temperature, by up to an order of magnitude.
- Summary: PM emissions were dominated by condensed material and having particle sizes of generally less than 100 nm.

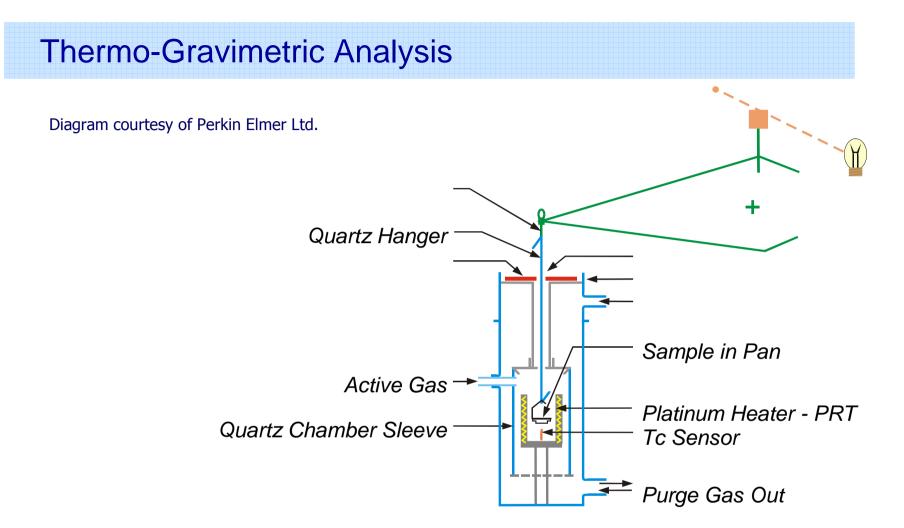


Thank you for listening

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Temperature ramp: 50 degC/min

Measure mass decrease as f(T) in inert atmosphere to get VOF mass fraction

Change atmosphere to an oxidising one to get EC mass fraction.



Results: Gas Phase Emissions

